National Exams May 2015

98-Pet-B5, Well Testing

3 hours duration

NOTES:

1. If doubt exists as to the interpretation of any question, the candidate is urged to submit with the answer paper, a clear statement of any assumptions made.

2. This is a CLOSED BOOK exam.

3. Any non-communicating calculator is permitted.

4. FIVE (5) questions constitute a complete exam paper.

5. The first five questions as they appear in the answer book will be marked.

6. All questions are of equal value unless otherwise stated and all parts in a multipart question have equal weight.

7. Clarity and organization of your answers are important, clearly explain your logic.

8. Pay close attention to units, some questions involve oilfield units, and these should be answered in the field units. Questions that are set in other units should be answered in the corresponding units.

9. A formula sheet is provided at the end of questions
Question 1 (20 Marks)

Explain (briefly in one or two sentences) the following concepts.

a) Infinite acting reservoir  
b) Non-Darcy flow  
c) Phase redistribution  
d) Dimensionless time  
e) Drill stem test  
f) Pseudo steady state  
g) Dual porosity reservoir  
h) Fall off test  
i) Drainage area  
j) Horner time

Question 2 (20 Marks)

An oil well is producing at a constant rate of 500 STBD in an infinite reservoir. The seismic survey indicates a sealing fault at 25 ft of the well. Calculate the wellbore pressure after 5 days.

Wellbore radius, $r_w = 0.25$ ft,  
Total compressibility, $c_t = 5 \times 10^{-5}$ psi$^{-1}$,  
Oil viscosity, $\mu_o = 2$ cP,  
Porosity, $\phi = 0.3$,  
Permeability, $k = 250$ mD,  
Formation thickness, $h = 20$ ft,  
Oil formation volume factor, $B_o = 1.2$ bbl/STB,  
Initial pressure, $p_i = 3000$ psi.
Question 3 (20 Marks)
A drawdown test has been conducted in an oil well and the following pressure data has been collected during the test. Estimate formation permeability and skin factor from the drawdown test data using the following reservoir and fluid properties. Required semi-log chart is given in the following.

Flow rate, $q = 90$ STBD,
Formation thickness, $h = 17$ ft,
Formation volume factor, $B_o = 1.1$ bbl/STB,
Initial reservoir pressure, $p_i = 1479$ psia,
Porosity, $\phi = 0.25$,
Total compressibility, $c_r = 7.65 \times 10^{-6}$ psi$^{-1}$,
Oil viscosity, $\mu_o = 7.86$ cP,
Wellbore radius, $r_w = 0.21$ ft.

<table>
<thead>
<tr>
<th>Time (hour)</th>
<th>$p_{wf}$ (psia)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>284</td>
</tr>
<tr>
<td>3</td>
<td>215</td>
</tr>
<tr>
<td>5</td>
<td>183</td>
</tr>
<tr>
<td>7</td>
<td>162</td>
</tr>
<tr>
<td>9</td>
<td>147</td>
</tr>
<tr>
<td>11</td>
<td>134</td>
</tr>
<tr>
<td>13</td>
<td>124</td>
</tr>
<tr>
<td>15</td>
<td>115</td>
</tr>
</tbody>
</table>
Question 4 (20 Marks)

Given the following test plots as well as formation and fluid properties for a gas reservoir, estimate the approximate end of wellbore storage, formation permeability and skin factor from the buildup test data using pseudo pressure method.

Flowing wellbore pressure prior to shut in, $p_{wf}=1378.84$ psia,
Pseudo pressure corresponding to $p_{wf}$, $p_{pwf}=1.77\times10^5$ psia$^2$/cp,
Formation thickness, $h=10$ ft,
Gas specific gravity, $\gamma=0.741$ (air = 1.0)
Wellbore radius, $r_w=0.46$ ft
Formation temperature, $T_f=108.9^\circ$F,
Porosity, $\phi=10.6\%$
Gas production rate, $q_g=8000$ MSCFD,
Total compressibility, $c_r=2.238 \times 10^{-4}$ psia$^{-1}$
Average gas viscosity $\mu_g=0.02$ cP
Production time prior to shut in, $t_p=72$ hr.
Question 5 (20 Marks)

A pressure build up has been conducted in an oil well in a naturally fractured reservoir. Pressure and derivative data are plotted in the following. Given the following formation and fluid properties estimate skin factor, initial reservoir pressure, and storativity (α) from the buildup test data.

Oil production rate, \( q = 125 \text{ STB/D} \),
Formation thickness, \( h = 17 \text{ ft} \),
Oil formation volume factor, \( B_o = 1.054 \text{ rb/STB} \),
Production time prior to shut in, \( t_p = 1200 \text{ hr} \),
Formation porosity, \( \phi = 13.0\% \),
Total compressibility, \( c_t = 7.19 \times 10^{-6} \text{ psi}^{-1} \),
Flowing wellbore pressure prior to shut in, \( p_{wf} = 211.20 \text{ psia} \),
Wellbore radius, \( r_w = 0.30 \text{ ft} \),
Oil viscosity, \( \mu_o = 1.72 \text{ cp} \).
Question 6 (20 Marks)

Pressure and derivative plots for a drawdown test in a hydraulically fractured well are shown in the following. Given the reservoir and fluid properties estimate fracture half-length and skin factor for this oil well. Assume an infinite conductivity hydraulic fracture. Required plots and chart are given in the following.

Oil rate, \( q = 200 \) STBD,
Reservoir permeability, \( k = 1.95 \) mD,
Formation thickness, \( h = 12 \) ft,
Oil formation volume factor, \( B_o = 1.325 \) bbl/STB,
Initial pressure, \( p_i = 3343.40 \) psia
Porosity, \( \phi = 11.8\% \),
Total compressibility, \( c_t = 14.7 \times 10^{-6} \) psi\(^{-1}\)
Wellbore radius, \( r_w = 0.25 \) ft
Oil viscosity, \( \mu_o = 0.49 \) cP.

<table>
<thead>
<tr>
<th>Time (hours)</th>
<th>( p_{wf} ) (psia)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.0000</td>
<td>3343</td>
</tr>
<tr>
<td>0.0010</td>
<td>3314</td>
</tr>
<tr>
<td>0.0040</td>
<td>3292</td>
</tr>
<tr>
<td>0.0090</td>
<td>3269</td>
</tr>
<tr>
<td>0.0128</td>
<td>3257</td>
</tr>
<tr>
<td>0.0239</td>
<td>3228</td>
</tr>
<tr>
<td>0.0320</td>
<td>3211</td>
</tr>
<tr>
<td>0.0426</td>
<td>3192</td>
</tr>
<tr>
<td>0.0564</td>
<td>3172</td>
</tr>
</tbody>
</table>
Question 7 (20 Marks)

A two-rate flow test has been conducted on a recently completed well in an undersaturated oil infinite acting reservoir. The well is produced at 25 STBD for 24 hours. The rate is then increased to 50 STBD for 72 hours. A flowing bottom hole wellbore pressure of 1000 psia has been recorded at the end of the second flow period (i.e., total test period of 96 hours).

The test was interpreted by a fellow reservoir engineer and a formation permeability of 162.6 mD and a skin factor of 2 have been estimated. Calculate the initial reservoir pressure. Required plot for calculations is given in the following.

Formation thickness, \( h = 50 \) ft,
Oil formation volume factor, \( B_o = 1.143 \) bbl/STB,
Porosity, \( \phi = 0.082, \)
Total compressibility, \( c_t = 10.5 \times 10^{-6} \) psi\(^{-1}\),
Oil viscosity, \( \mu_o = 1.278 \) cp,
Wellbore radius, \( r_w = 0.45 \) ft.
\[ p_D = 0.5 [ - \text{Ei}(1/4t_D) ] \]

Plot of dimensionless pressure versus dimensionless time
Formula Sheet

Slope of semi-log straight line, psi/cycle: \( m = \frac{162.6q\mu B_o}{kh} \)

Radius of investigation, ft: \( r \approx \sqrt{\frac{kt}{948\phi \mu c_i}} \)

Permeability-thickness product for double porosity reservoirs, mD-ft \((kh)_J = \hat{k}_J h = \frac{162.6q\mu B}{m}\)

Average fracture permeability, mD \( \hat{k}_J = \frac{\hat{k}_J h}{h} \)

Skin factor for buildup test: \( S = 1.151 \left( \frac{p_{1hr} - p_{w,fr} (\Delta t = 0)}{m} \right) \frac{\log \left( \frac{k}{\phi \mu c, r^2_w} \right)}{+ 3.23} \)

Skin factor for drawdown test: \( S = 1.151 \left( \frac{p_i - p_{1hr}}{m} \right) \frac{\log \left( \frac{k}{\phi \mu c, r^2_w} \right)}{+ 3.23} \)

Pseudo steady state equations: \( \frac{dp_w}{dt} = -\frac{0.234 q B_o}{c_i V_p}, \quad \text{(psi/hr)} \)

\( p(r_w, t) = p_i - \frac{0.0744 q B_o t}{\phi c_i h r^2} + \frac{q \mu B_o}{0.00708kh} \left[ \ln \left( \frac{r_s}{r_w} \right) - \frac{3}{4} + S \right] \)

Horner time ratio: \( \frac{t_p + \Delta t}{\Delta t} \)

Distance to fault, ft: \( L = \sqrt{\frac{0.000148 k \Delta t}{\phi \mu c_i}} \)

The approximate time required for the slope to double, hr \( \Delta t = \frac{3.8 \times 10^5 \phi \mu c_i L^2}{k} \)

\( p(r, t) = p_i - \frac{q \mu B_o}{0.00708kh} P_D, \quad \eta = \frac{0.002637k}{\phi \mu c_i}, \quad t_D = \frac{\eta t}{r^2} \)

\( P_D = \frac{1}{2} (\ln t_D + 0.809) \) only if \( t_D > 100 \), for \( t_D < 100 \) use the provide \( P_D \) graph.

\( p(r, t) = p_i - \frac{0.141 q \mu B_o}{kh} (P_D + S) \)

Gas wells build up

\( m = \frac{1637q\Delta T}{kh} \)

\( S' = 1.151 \left( \frac{P_{1hr} - P_{w,fr} (\Delta t = 0)}{m} \right) \frac{\log \left( \frac{k}{\phi \mu c, r^2_w} \right)}{+ 3.23} \)

Fracture half length
\[ L_f = \frac{4.064qB_o}{m h \sqrt{k}} \left( \frac{\mu_o}{\phi c_i} \right)^{0.3}, \quad L_f = 2r_w e^{-s} \]

**Nomenclature**

- \( B_o \): Oil formation volume factor, bbl/STB
- \( c_i \): Total compressibility, 1/psi
- \( h \): Formation thickness, ft
- \( k \): Permeability, mD
- \( L \): Distance, ft
- \( p \): Pressure, psia
- \( p_p \): Pseudo pressure, psia²/cP
- \( q \): Oil flow rate, STBD
- \( q_g \): Gas flow rate, MSCFD
- \( r \): Radius, ft
- \( S \): Skin factor, dimensionless
- \( T \): Temperature, Rankin
- \( t \): Time, hr
- \( V_p \): Pore volume, ft³

- \( \phi \): Porosity, fraction
- \( \mu \): Oil viscosity, cP
- \( \eta \): Hydraulic diffusivity, ft²/hr

**Subscripts**

- \( D \): dimensionless
- \( e \): external
- \( f \): fracture
- \( i \): initial
- \( o \): oil
- \( p \): production
- \( t \): total
- \( w \): wellbore

**Conversion Factors**

- 1 m³ = 6.28981 bbl = 35.3147 ft³
- 1 acre = 43560 ft²
- 1 ac-ft = 7758 bbl
- 1 Darcy = 9.869233 × 10⁻¹³ m²
- 1 atm = 14.6959488 psi = 101.32500 kPa = 1.01325 bar
- 1 cP = 0.001 Pa·sec
- 1 m = 3.28084 ft = 39.3701 inch